

## Supplementary Information for “Normal stress anisotropy and marginal stability in athermal elastic networks”

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### Affinely deforming isotropic network models

Consider a filament segment with initial orientation  $\hat{\mathbf{n}}$ , undergoing deformation described by the tensor  $\mathbf{\Lambda}(\gamma)$ . The deformation changes the filament’s length and orientation, resulting in a tension  $\boldsymbol{\tau}$  directed along its new orientation. Treating the filament as a linear elastic element with stretching modulus  $\mu$  and initial length  $l_0 = 1$ , the tension vector is  $\boldsymbol{\tau} = \tau \mathbf{\Lambda} \hat{\mathbf{n}} / |\mathbf{\Lambda} \hat{\mathbf{n}}|$ . For the spring model, we utilize a linear Hookean force-extension relation in which the filaments support both tension and compression:  $\tau = \tau_s$  where  $\tau_s = \mu(|\mathbf{\Lambda} \hat{\mathbf{n}}| - 1)$ . For the rope model, we instead use a one-sided force-extension relation that is only finite under tension:  $\tau = \tau_r$ , with

$$\tau_r = \begin{cases} \mu(|\mathbf{\Lambda} \hat{\mathbf{n}}| - 1) & (|\mathbf{\Lambda} \hat{\mathbf{n}}| > 1) \\ 0 & (|\mathbf{\Lambda} \hat{\mathbf{n}}| \leq 1) \end{cases}. \quad (1)$$

Taking the average, over all initial filament orientations, of the product of the  $i$  component of the tension,  $\tau \Lambda_{il} n_l / |\mathbf{\Lambda} \hat{\mathbf{n}}|$ , and the line density of filaments crossing the  $j$  plane after the deformation,  $\frac{\rho}{\det \mathbf{\Lambda}} \Lambda_{jk} n_k$ , yields the stress tensor [1, 2],

$$\sigma_{ij} = \frac{\rho}{\det \mathbf{\Lambda}} \left\langle \tau \frac{\Lambda_{il} n_l \Lambda_{jk} n_k}{|\mathbf{\Lambda} \hat{\mathbf{n}}|} \right\rangle. \quad (2)$$

Since we consider only volume-conserving simple shear,  $\det \mathbf{\Lambda} = 1$ . Thus, for filaments in 3D with initial polar angle  $\theta$  and azimuthal angle  $\varphi$ , the stress tensor is

$$\sigma_{ij} = \frac{\rho}{4\pi} \int_{\varphi} \int_{\theta} d\theta d\varphi \sin \theta \left[ \tau \frac{\Lambda_{il} n_l \Lambda_{jk} n_k}{|\mathbf{\Lambda} \hat{\mathbf{n}}|} \right], \quad (3)$$

in which the deformation tensor for simple shear in 3D is

$$\mathbf{\Lambda}(\gamma) = \begin{pmatrix} 1 & 0 & \gamma \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad (4)$$

and the transformed orientation vector is

$$\mathbf{\Lambda} \hat{\mathbf{n}} = \begin{pmatrix} \sin \theta \cos \varphi + \gamma \cos \theta \\ \sin \theta \sin \varphi \\ \cos \theta \end{pmatrix}. \quad (5)$$

We compute the  $xz$ ,  $xx$ , and  $zz$  components of the stress tensor for the 3D case as follows:

$$\sigma_{xz} = \frac{\rho}{4\pi} \int_{\varphi} \int_{\theta} d\theta d\varphi \sin \theta \left[ \tau \frac{(\sin \theta \cos \varphi + \gamma \cos \theta) \cos \theta}{|\mathbf{\Lambda} \hat{\mathbf{n}}|} \right] \quad (6)$$

$$\sigma_{xx} = \frac{\rho}{4\pi} \int_{\varphi} \int_{\theta} d\theta d\varphi \sin \theta \left[ \tau \frac{(\sin \theta \cos \varphi + \gamma \cos \theta)^2}{|\mathbf{\Lambda} \hat{\mathbf{n}}|} \right] \quad (7)$$

$$\sigma_{zz} = \frac{\rho}{4\pi} \int_{\varphi} \int_{\theta} d\theta d\varphi \sin \theta \left[ \tau \frac{\cos^2 \theta}{|\mathbf{\Lambda} \hat{\mathbf{n}}|} \right] \quad (8)$$

The integrals are taken over the ranges  $0 \leq \theta \leq 2\pi$  and  $0 \leq \varphi \leq \pi$ . To compare with our results for the 3D FCC network, we use  $\mu = 1$  and initial line density  $\rho = \frac{12}{\sqrt{2}}$ , corresponding to the fully-connected FCC lattice with  $l_0 = 1$  [3].

We repeat the same process for the 2D case, in which the deformation tensor for simple shear is

$$\mathbf{\Lambda}(\gamma) = \begin{pmatrix} 1 & \gamma \\ 0 & 1 \end{pmatrix} \quad (9)$$

and the transformed orientation vector is

$$\mathbf{\Lambda} \hat{\mathbf{n}} = \begin{pmatrix} \cos \theta + \gamma \sin \theta \\ \sin \theta \end{pmatrix}. \quad (10)$$

The resulting components of the 2D stress tensor are calculated as follows:

$$\sigma_{xz} = \frac{\rho}{2\pi} \int_{\theta} d\theta \left[ \tau \frac{(\cos \theta + \gamma \sin \theta) \sin \theta}{|\mathbf{\Lambda} \hat{\mathbf{n}}|} \right] \quad (11)$$

$$\sigma_{xx} = \frac{\rho}{2\pi} \int_{\theta} d\theta \left[ \tau \frac{(\cos \theta + \gamma \sin \theta)^2}{|\mathbf{\Lambda} \hat{\mathbf{n}}|} \right] \quad (12)$$

$$\sigma_{zz} = \frac{\rho}{2\pi} \int_{\theta} d\theta \left[ \tau \frac{\sin^2 \theta}{|\mathbf{\Lambda} \hat{\mathbf{n}}|} \right] \quad (13)$$

Here, the integrals are taken over the range  $0 \leq \theta \leq 2\pi$ .

### Principal strain axes for simple shear

For simple shear with deformation gradient tensor

$$\mathbf{\Lambda}(\gamma) = \begin{pmatrix} 1 & 0 & \gamma \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}, \quad (14)$$

we can decompose  $\mathbf{\Lambda}$  into a combination of a pure stretch  $\mathbf{U}$  and a rigid body rotation  $\mathbf{R}$ , satisfying  $\mathbf{\Lambda} = \mathbf{R}\mathbf{U}$ . From the right Cauchy-Green tensor  $\mathbf{C} = \mathbf{U}^2 = \mathbf{\Lambda}^T \mathbf{\Lambda}$ , we determine

$$\mathbf{U} = \frac{1}{\sqrt{4 + \gamma^2}} \begin{pmatrix} 2 & 0 & \gamma \\ 0 & \sqrt{4 + \gamma^2} & 0 \\ \gamma & 0 & 2 + \gamma^2 \end{pmatrix}. \quad (15)$$

The eigenvalues of  $U$  are

$$\lambda_1 = \frac{\gamma + \sqrt{\gamma^2 + 4}}{2}, \quad \lambda_2 = \frac{-\gamma + \sqrt{\gamma^2 + 4}}{2}, \quad \lambda_3 = 1 \quad (16)$$

with corresponding eigenvectors

$$\mathbf{v}_1 = \left( \frac{1}{2} \left( -\gamma + \sqrt{4 + \gamma^2} \right), 0, 1 \right)$$

$$\mathbf{v}_2 = \left( \frac{1}{2} \left( -\gamma - \sqrt{4 + \gamma^2} \right), 0, 1 \right)$$

$$\mathbf{v}_3 = (0, 1, 0)$$

$\lambda_1$  and  $\lambda_2$  correspond to the elongation  $l/l_0$  along the axes of maximum extension and compression, respectively.

The rotation matrix  $\mathbf{R}$  is determined as  $\mathbf{R} = \mathbf{\Lambda}U^{-1}$ ,

$$\mathbf{R} = \frac{1}{\sqrt{4 + \gamma^2}} \begin{pmatrix} 2 & 0 & \gamma \\ 0 & \sqrt{4 + \gamma^2} & 0 \\ -\gamma & 0 & 2 \end{pmatrix} \quad (17)$$

The maximum stretch direction then corresponds to  $\mathbf{v}'_1 = \mathbf{R}\mathbf{v}_1$ . In the limit of small strains,  $\mathbf{v}'_1$  is oriented at  $\theta = \pi/4$  above the  $x$ -axis, in the  $x$ - $z$  plane.

## Bending interaction models

Prior work has shown that network models with bond-bending interactions (angle constraints between all nearest-neighbor bonds) exhibit the same strain-driven critical behavior as networks with freely-hinging crosslinks (angle constraints between only initially collinear nearest-neighbor bonds) [4, 5]. To emphasize that the details of the bending interactions do not influence our conclusions with regard to the normal stresses, we consider the mechanics of phantomized triangular networks with  $z = 3.4$  and either freely-hinging crosslinks (bending along initially collinear fibers) or bond-bending interactions, both with  $\tilde{\kappa} = 10^{-5}$ . In Fig. S1, we show both  $K$  and the normal stresses  $\sigma_{ii}/\gamma^2$  for each bending interaction type. We observe that the networks show qualitatively similar behavior in both cases, with  $K \propto \tilde{\kappa}$  and  $\sigma_{ii} \propto \tilde{\kappa}\gamma^2$  below the critical strain. The only apparent difference is that the magnitudes of  $K$  and the normal stresses are slightly higher for bond-bending networks than for networks with freely-hinging crosslinks in the bending-dominated regime. This is due to the additional angle constraints imposed by bond-bending interactions.

## Packing-derived networks with varying connectivity

In Fig. S2, we show both  $N_1/(\sigma_{xz}\gamma)$  and  $K$  for 2D packing-derived networks of size  $W = 100$  with  $\kappa = 10^{-5}$  and varying  $z$ . We observe that, for individual samples, peaks in  $N_1/(\sigma_{xz}\gamma)$  occur at the  $z$ -dependent critical strain. On average, the Lodge-Meissner relation is satisfied.

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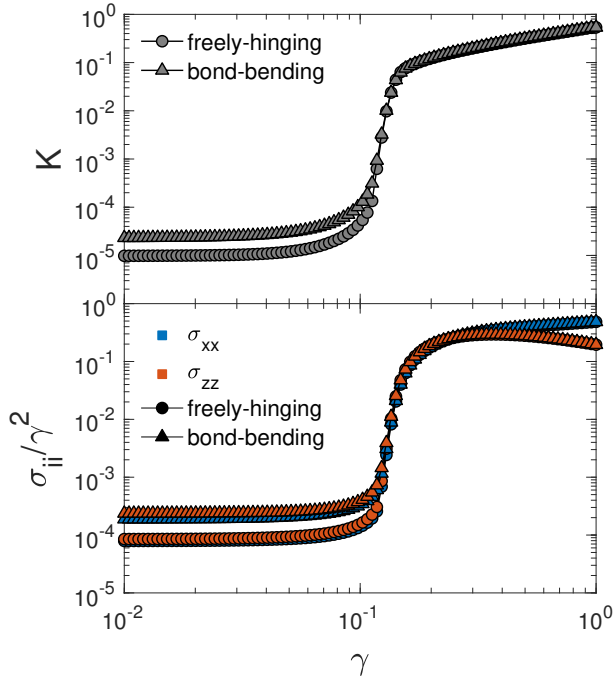


FIG. S1. Top: Differential shear modulus  $K$  vs. shear strain  $\gamma$  for 2D phantomized triangular networks with  $z = 3.4$ ,  $\bar{\kappa} = 10^{-6}$  and  $\delta_{\max} = 0.4$ , with freely-hinging crosslinks and bending interactions only along fibers (triangles) and with bond-bending interactions between all nearest-neighbor bonds (circles). Bottom: Normal stresses  $\sigma_{xx}$  and  $\sigma_{zz}$ , both normalized by  $\gamma^2$ , as a function of  $\gamma$  for the same systems. Both  $K$  and  $\sigma_{ii}$  are higher in networks with bond-bending interactions than in the same networks with freely-hinging crosslinks, due to the additional angle constraints.

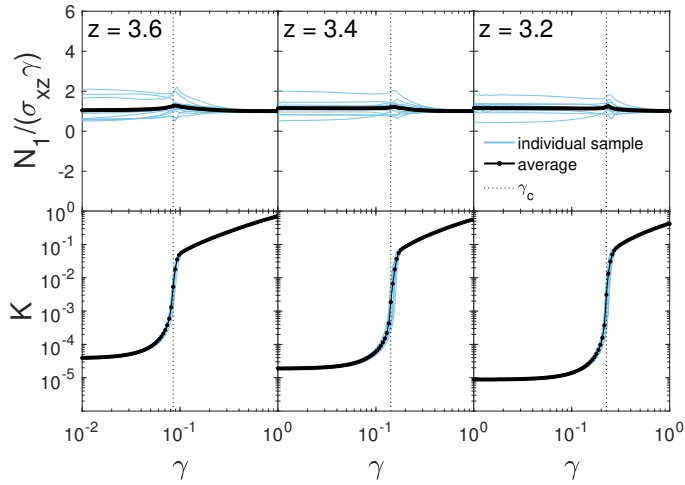


FIG. S2. In 2D packing-derived networks with  $\kappa = 10^{-5}$  and varying  $z$ , we observe either upward or downward peaks in  $N_1/(\sigma_{xz}\gamma)$  (top) for individual samples at the  $z$ -dependent critical strain  $\gamma_c$ , determined as the inflection point of  $K$  vs  $\gamma$  (bottom) plotted on a logarithmic scale. When the stress is averaged over all samples, the network ensemble approximately satisfies the Lodge-Meissner relation, such that  $N_1/(\sigma_{xz}\gamma) = 1$  over the full strain range.